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# On the compression behavior of $Ti_2InC$ , $(Ti_{0.5}, Zr_{0.5})_2InC$ , and $M_2SnC$ (M = Ti, Nb, Hf) to quasi-hydrostatic pressures up to 50 GPa

Bouchaib Manoun a,b,\*, O.D. Leaffer C, S. Gupta C, E.N. Hoffman C, S.K. Saxena D, J.E. Spanier C, M.W. Barsoum C

- <sup>a</sup> Laboratoire de Physico-Chimie des Matériaux, Département de Chimie, FST Errachidia, University Moulay Ismail, Morocco
- <sup>b</sup> Center for Study of Matter at Extreme Conditions, Florida International University, VH-140, University Park, Miami, FL 33199, USA
- <sup>c</sup> Department of Materials Science and Engineering, Drexel University, Philadelphia, PA 19104, USA

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#### ABSTRACT

Using a synchrotron X-ray radiation source and a diamond anvil cell we measured the dependences of the lattice parameters on quasi-hydrostatic pressure of the order of 50 GPa of the following MAX phases:  $Ti_2InC$ ,  $(Ti_{0.5}, Zr_{0.5})_2InC$ ,  $Zr_2InC$  and  $Ti_2SnC$ ,  $Nb_2InC$  and  $Hf_2InC$ . Like other MAX phases, the phases studied herein were all stable up to  $\approx$ 50 GPa. In both series, the substitution of Ti (r=1.32 Å) by the larger sized metals, Zr or Nb (with r varying between 1.34 and 1.55 Å) resulted in larger unit cell parameters and volumes. At  $152\pm3$  and  $148\pm3$  GPa, the respective bulk moduli,  $K_0$ , of  $Ti_2SnC$  and  $Ti_2InC$  are quite comparable. Replacing Ti by Ti or  $Ti_2SnC$  leads to increases in Ti oby 11% and 18%, respectively. Conversely, replacing half the Ti by Ti or  $Ti_2InC$  leads to a 13% drop in Ti or T

## 1. Introduction

The  $M_{n+1}AX_n$  (MAX) compounds, where n=1,2 or 3, M is an early transition metal, A is an A-group (mostly IIIA and IVA) element, and X is C or N, have been studied extensively these last few years [1–9]. These compounds adopt a hexagonal crystal structure (space group  $P6_3/mmc$ ), with two formula units per unit cell, consisting of layers of edge-sharing MC<sub>6</sub> octahedra interleaved with square-planar A layers. The octahedra are identical to those found in the rock salt structure of the corresponding binary compounds, MX [10]. The phases studied in this work belong to the n=2, or 211, subgroup.

The MAX phases have been widely studied due to their commercial potential. Most are good thermal and electrical conductors, damage tolerant and thermal shock resistant. They are relatively soft (Vickers hardness  $\approx 2-8$  GPa) and readily machinable [11]. Some of them, most notably  $\text{Ti}_3\text{SiC}_2$  and  $\text{Ti}_2\text{AlC}$ , are promising candidates for high-temperature structural

applications, because of their high-temperature strengths and good oxidation resistance even under severe thermal cycling [12]. Many are elastically quite stiff, with densities comparable to that of Ti metal, and Debye temperatures (700 K) that are quite high [13–15]. This combination of properties derives partially from the metallic nature of the bonding, partially from the layered nature of the structure and partially from the fact that basal plane dislocations are mobile at all temperatures. We have also recently shown that the attenuation of sound waves in Ti<sub>2</sub>AlC was higher than that of many woods and comparable to that of some polymers [16,17].

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Over the last few years a concerted effort has been made to try to understand the relationship between MAX phase chemistries and their mechanical and elastic properties. Most germane to this paper are the isothermal bulk moduli,  $K_0$ . Manoun et al. [18–25] reported the  $K_0$  values of  $M_2$ AlC (M=Ti,V,Cr,Nb and Ta) [18],  $Ti_3Si_{0.5}Ge_{0.5}C_2$  [19],  $Zr_2InC$  [20],  $Ti_4AIN_3$  [21],  $Ta_4AIC_3$  [22],  $Ti_3AICN$  [23],  $Ti_3(AI,Sn_{0.2})C_2$  [23], TiVAIC and TiNbAIC [24],  $Cr_2GeC$  and  $V_2GeC$  [25]. In all cases, like in  $Ti_3SiC_2$  [26], no phase transitions were observed up to pressures of the order of 55 GPa.  $K_0$  of these compounds varied from a high of 261 GPa for  $Ta_4AIC_3$  [22], to a low of 127 GPa for  $Zr_2InC$  [20]. For the most part, the relative shrinkage along the c-direction with pressure was greater than

<sup>\*</sup> Corresponding author at: Center for Study of Matter at Extreme Conditions, Florida International University, VH-140, University Park, Miami, FL 33199, USA. E-mail address: bmanoun@yahoo.com (B. Manoun).

along the *a*-direction; the exceptions were Cr<sub>2</sub>AlC, Nb<sub>2</sub>AlC [18], and Nb<sub>2</sub>AsC [27], where the opposite was true. The Ta-containing phases were unique in that the shrinkages along both directions were quite similar [18,22].

More recently we have shown that replacing C by N in  $Ti_2AlC$  results in a decrease in  $K_0$ , presumably because of the formation of vacancies on the N and/or Al sites [28]. Replacing Ge by Si in  $Ti_3GeC_2$ , on the other hand, does not affect  $K_0$  greatly [29]. Replacing Nb by Ti in Nb<sub>2</sub>AlC, or V by Ti in V<sub>2</sub>AlC, resulted in a decrease in  $K_0$  of the solid solution compositions relative to the end members [24].

The combination of easy machinability, relatively low densities (of some of the phases) and high elastic constants, together with the possibility of extremely high damping [16,17] is one that to date had not been possible. Herein we explore the effects of the M-site chemistry on  $K_0$ . More specifically, we studied the following phases:  $Ti_2SnC$ ,  $Nb_2SnC$ ,  $Hf_2SnC$ ,  $Ti_2lnC$  and  $(Ti_{0.5}, Zr_{0.5})_2lnC$ , henceforth referred to as TiZrlnC. The results of the In-containing compounds are compared to  $K_0$  of  $Zr_2lnC$  measured previously [20]. Further motivation is our interest in exploring the stability of these phases at high pressures as well as a general understanding of their structure/chemistry/property relationships.

#### 2. Experimental details

The processing details for the  $M_2SnC$  (M=Ti,Nb,Hf) compounds can be found elsewhere [30]. In brief, stoichiometric proportions of the Ti, Nb, Hf, Sn and C powders were mixed, cold pressed and sealed in borosilicate glass tubes that were then heated, in a hot isostatic press (HIP), at a rate of 5 °C/min to 850 °C, a temperature at which the glass tubes soften. Upon reaching 850 °C, the HIP was pressurized to 55 MPa and heating was resumed at the same heating rate to the processing temperature, at which point the pressure in the HIP increased to 60–70 MPa. The various compositions were held at the processing temperatures (1250–1325 °C) for different times, varying from 4–24 h [30].

The processing details of the In-containing compounds can also be found elsewhere [31,32]. In brief, stoichiometric proportions of the Ti, Zr, In and C powders were mixed, sealed in borosilicate glass tubes under a mechanical vacuum and heated to 650 °C for 10 h before furnace cooling. This procedure collapsed the tubes and allowed the powders to pre-react. The collapsed tubes were placed in a HIP and heated to 750 °C, at which time the HIP was pressurized to  $\approx$ 70 MPa before the heating was resumed to a temperature of 1300 °C. Typically the samples were held at temperature for 12 h [31,32].

The X-ray diffraction (XRD) patterns for Ti<sub>2</sub>InC, TiZrInC and  $M_2SnC$  (M  $\,=\,$  Ti, Nb) were collected at the high-pressure collaborative access team (HPCAT) beam line at the advanced photon source (Argonne National Laboratory, Chicago, IL). A monochromatic beam – with a wavelength of 0.4066 Å – was focused to a 10  $\mu m$  spot size on the sample. Diffraction rings were recorded between  $2\theta=1^\circ$  and  $35^\circ$  using an image plate.

For Hf<sub>2</sub>SnC, the diffraction patterns were collected using an energy-dispersive mode at the bending magnet beamline of the Cornell High-Energy Synchrotron Source (CHESS). A solid state Ge detector, used to detect the diffracted energy, was calibrated with fluorescence standards of  $^{55}$ Fe and  $^{133}$ Ba, while the  $2\theta_0$  of  $10^\circ$  was attuned taking diffraction patterns of a gold standard.

Measurements were conducted at room temperature; powdered samples were pressurized using a gasketed diamond anvil cell (DAC) with a 300  $\mu$ m culet. A 250  $\mu$ m initial thickness rhenium gasket was indented to about 50–60  $\mu$ m.

The stress state of a sample compressed in a DAC can become non-hydrostatic if the material tested is hard and has low compressibility, like the MAX phases. However, it has been shown that the sample pressure can be rendered nearly hydrostatic by using a large volume of a low shear strength material as the pressure-transmitting medium. We have repeatedly shown that Al – with its low shear modulus and lack of phase transitions – was a good pressure-transmitting medium [18–25,28,29,33,34]. Another advantage of Al is the fact that its pressure–volume relationship is well established [35]. In this work, powdered samples were placed between two 15  $\mu m$  thick Al foils, before packing them in the 100–150  $\mu m$  hole in the Re gasket. More details can be found in any of our previous papers [18–25,28,29].

The FIT2D software [36,37] was employed to convert the image plate records into  $2\theta$ 's and intensities. The a and c lattice cell parameters were determined using least squares refinement on individually fitted peaks.

The bulk moduli were computed using ab initio density functional calculations, conducted using the Vienna Ab initio Simulation Package (VASP) [38] with the MedeA [39] interface. All calculations were carried out using the projector augmented wave (PAW) [40,41] and the generalized gradient approximation (GGA) [42]. Relaxed structures were calculated and energies were converged with respect to the *k*-mesh using MedeA's convergence method. Subsequent calculations were carried out using the *k*-mesh resulting from the convergence. The bulk moduli were calculated using the method outlined in Ref. [43], which in summary consisted of calculating the volume of the relaxed unit cell and then calculating the energy of the unit cell relaxed with the additional condition that the volume be fixed. The relationship between the energy and the volume was then used to determine the bulk moduli using the Birch-Murnaghan equation [44,45].

### 3. Results

The XRD spectra and their pressure dependences are shown in Fig. 1a–f. The space group adopted for all phases is  $P6_3/mmc$ , and the lattice parameters obtained (Table 1) are in good agreement with previous work.

Fig. 2 plots the variations in relative unit cell volumes,  $V/V_o$ , as a function of applied quasi-hydrostatic pressure P.  $V_o$  is volume of unit cell when P=1 atm. Second-order polynomial least square fits of these data resulted in the coefficients listed in Table 2. Fitting the same results to the Birch–Murnaghan equation [45]

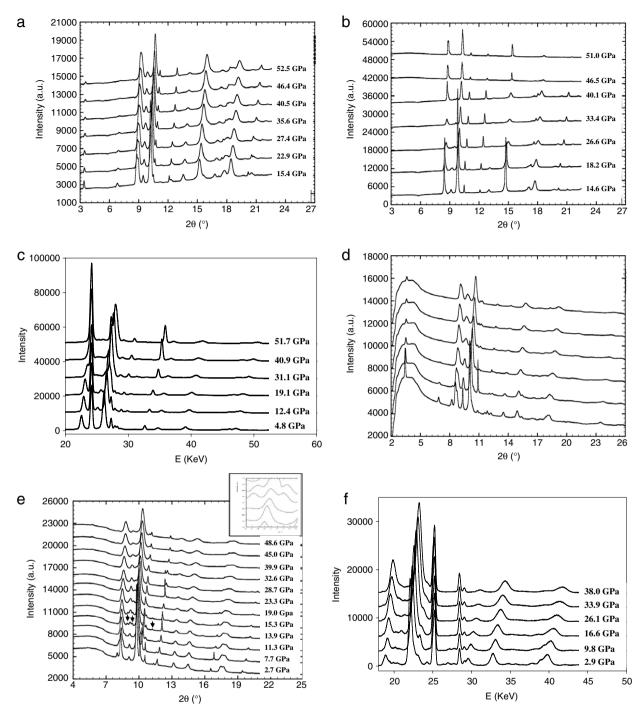
$$P = 3/2K_o[(V/V_o)^{-7/3} - (V/V_o)^{-5/3}] \times [1 + 3/4(K'_o - 4)[(V/V_o)^{-2/3} - 1]]$$

yields  $K_0$  values of 148  $\pm$  3 GPa for Ti<sub>2</sub>InC and 131  $\pm$  3 GPa for TiZrInC. For the M<sub>2</sub>SnC compounds,  $K_0$  was 152  $\pm$  3 GPa for Ti<sub>2</sub>SnC, 169  $\pm$  4 GPa for Hf<sub>2</sub>SnC and 180  $\pm$  5 GPa for Nb<sub>2</sub>SnC. It follows, not surprisingly, that the  $K_0$  values reported herein are in line with previous MAX phase results in that these solids are elastically quite stiff.

Fig. 3 plots the relative changes in lattice parameters,  $a/a_o$  and  $c/c_o$ , as a function of P. The subscripts refer to the values of a and c when P=1 atm. Note that for all compositions the contraction along the c-direction is greater than that along the a-direction. Second-order polynomial least square fits of these data resulted in the coefficients listed in Table 3.

#### 4. Discussion

The lattice parameters reported herein are in good agreement with previous work (Table 1). When these, and related lattice parameters, are plotted versus the atomic radii,  $r_M$ , of the M elements (Fig. 4) a somewhat complicated picture emerges. (In Fig. 4,  $r_M$  for the solid solutions was taken to be the average of the end members' radii. Also, the y-axis scales were chosen



**Fig. 1.** Functional dependence of high-pressure XRD spectra for (a) Ti<sub>2</sub>InC, (b) TiZrInC, (c) Zr<sub>2</sub>InC, (d) Ti<sub>2</sub>SnC, (e) Nb<sub>2</sub>SnC and (f) Hf<sub>2</sub>SnC on quasi-hydrostatic pressure, *P*. Upon compression, most peaks remain visible until the highest pressures reached. With increasing *P*, the peaks become broader, lose intensity, and some merge together. In Fig. 1e the arrows point to extra reflections that do not belong to Nb<sub>2</sub>SnC; the inset show the additional reflections.

to reflect the same percentage change in the lattice parameters.) To make sense of the results, we focus first on the In series (Fig. 4a). Here two sets of lines emanate from the  $Ti_2InC$  corner, one joining  $Hf_2InC$ , and the other, at a steeper slope, joining  $Hf_2InC$ . Not surprisingly, the TiHflnC lattice parameters follow Vegard's law, i.e. they fall on the Ti–Hf line. Interestingly, but consistent with our ab initio calculations (Table 1), the lattice parameters of the Hf-containing compounds are lower than those for the Zr-containing ones, despite the fact that the radius of Hf is larger than that of Zr. The  $Nb_2InC$  results are intriguing, however. The a-lattice parameter (red symbols, left y-axis) fall on the Ti–Hf line; the c-

lattice parameter (black symbols, right y-axis) on the Ti–Zr line. The identical behavior is seen for Nb<sub>2</sub>SnC in the M<sub>2</sub>SnC system (Fig. 4b).

The situation for the Sn-containing compounds is similar; the lines joining the respective parameters of  $Ti_2SnC$  to  $Zr_2SnC$  are steeper than the ones joining  $Ti_2SnC$  to  $Hf_2SnC$ . The lattice parameters of  $Zr_2SnC$  (a=3.358 Å and c=14.57 Å) were taken from Ref. [30].

For the most part, most peaks remain visible until the highest pressures reached (Fig. 1). With increasing pressure, the peaks become broader, lose intensity, and some merge together. Except for Nb<sub>2</sub>SnC, no extra peaks appear in the patterns up to  $\approx$ 50 GPa, a